

Electronic Supplementary Information (ESI) for

A similarity scaling approach for organ-on-chip devices

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The main paper proposes similarity scaling as a systematic method for scaling organ-on-chip (OoC) devices. In the following, we first illustrate the technique of dimensional analysis with an example, and then carry out the detailed analysis for each of the 3 case studies of the main text, with all supporting data.

Dimensional analysis

Dimensional analysis and similarity are widely used in science and engineering [1]. The procedure is underpinned by the pi theorem, and reduces the functional dependence of an output quantity P on the inputs q_1, \dots, q_n of a problem

$$P = f(q_1, q_2, \dots, q_n)$$

to an equivalent functional relationship among a smaller number of dimensionless groups, called the Π groups:

$$\Pi_1 = F(\Pi_2, \dots, \Pi_m),$$

where Π_1 is the dimensionless group containing the output P , and the other Π groups contain the input variables and parameters. The functional form F

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generally differs from f , and the second equation involves a smaller number of variables: $m < n + 1$.

Consider a physical or biological systems such as an organ (to be called a “prototype” below), alongside a “model” that is typically a scaled down *in vitro* version of the prototype. The dimensional analysis can be performed on both, resulting in relationships among the Π groups. Provided that the model operates from the same underlying mechanisms and principles as the prototype, the functional form F is the same between them. Therefore, if we control the operating conditions and parameters in the model system so that its input Π groups ($\Pi_2, \dots \Pi_m$) match those of the prototype, then the output Π_1 must match as well:

$$\Pi_1^{model} = \Pi_1^{prototype},$$

which allows us to scale the measured values in the model system to that in the prototype. The model and prototype are said to be in similarity.

The procedure of constructing the Π groups is detailed in textbooks; Zlokarnik [1] is a highly readable one with many examples. The key is to recognize that the dimensions of all the variables and parameters of a problem consist of a few fundamental dimensions such as length, mass, time, temperature, amount of substance and electric charge. Thus, a judicious combination of these variables and parameters, through multiplication, division and exponentiation, will yield a dimensionless group. The total number of dimensionless groups is typically the number of variables and parameters minus the number of fundamental dimensions. All such Π groups can be derived through a systematic and foolproof procedure [1]. In the following, we will illustrate this through an example.

An example from engineering

As an illustration of the procedure, let us consider a classical example from aeronautics. If we design an experiment to study the drag force D on an aircraft, we build a model of the plane—much smaller than the prototype—and blow wind over the model in a wind tunnel. Thus, one can measure D on the model.

The starting point of the dimensional analysis is to list all the variables and parameters of the problem that may have affected the quantity of main interest that we have measured. Here, we take D to be dependent on the air density ρ , air viscosity μ , wind speed U and the dimension d of the airplane. Of course, there may be multiple dimensions for the airplane, e.g., length, width and height. We use a single dimension d for simplicity in this illustration. Thus, we list D as the output and the other 4 quantities as inputs: ρ, μ, U, d .

Next, we express the dimension of each of the variables in terms of the 3 fundamental dimensions of the problem: length (L), time (T) and mass (M). For example, D is a force, whose dimension is mass times length divided by time

squared (from Newton's second law of motion): $\{D_f\} = \text{MLT}^{-2}$. Similarly we write out the dimensions for all the other variables and parameters, based on the physical meaning of each quantity (e.g., viscosity as defined from the shear stress on a Newtonian fluid):

Outputs: $\{D_f\} = \text{MLT}^{-2}$; Inputs: $\{\rho\} = \text{ML}^{-3}$, $\{\mu\} = \text{ML}^{-1}\text{T}^{-1}$, $\{U\} = \text{LT}^{-1}$, $\{d\} = \text{L}$.

Because there are 3 fundamental dimensions, if we combine 4 quantities together via multiplication, division and exponentiation, we should be able to cancel out the 3 fundamental dimensions to produce a Π group. Let us try this among the 4 inputs:

$$\Pi_2 = \rho^a \mu^b U^c d,$$

with the exponents a , b and c being numbers to be determined. We call this group Π_2 as we have on p. 1 reserved Π_1 for the dimensionless group involving the output quantity (D in this case; see below). Requiring the dimension of Π_2 to vanish gives 3 algebraic equations for a , b and c :

$$\{\Pi_2\} = (\text{ML}^{-3})^a (\text{ML}^{-1}\text{T}^{-1})^b \{\text{LT}^{-1}\}^c \text{L} = \text{M}^0 \text{L}^0 \text{T}^0$$

The unique solution is $a = 1$, $b = -1$ and $c = 1$. Thus, we obtain

$$\Pi_2 = \rho U d / \mu,$$

which is known as the Reynolds number Re , widely used in fluid dynamics. A combination of the output D with three inputs, e.g., ρ , U , d , leads to another Π group:

$$\Pi_1 = D / (\rho U^2 d^2),$$

which is commonly known as the drag coefficient C_d . From the above procedure, we make the following observations:

- Because there are 3 fundamental dimensions and 5 variables and parameters, there are $5 - 3 = 2$ independent dimensionless Π groups for this problems.
- The Π groups are not unique; any product or quotient of any powers of the Π groups makes a new Π group, which is however not independent of the original 2. If we had tried to form a Π group from D , U , d and μ , for example, we would have ended up with $\Pi_3 = D / (\mu U d) = \Pi_1 \cdot \Pi_2$.
- The choice of which Π groups to use depends on the need of the problem and convention. A rule of thumb is to form one Π group for each of the output variables of interest. This facilitates the analysis and plotting of dimensionless data.

Now the pi theorem stipulates that the dependence of D on the inputs can be reduced to a simpler dependence among the Π groups: $C_d = F(Re)$. In fact, graphs of the drag coefficient as a function of the Reynolds number are widely available on aircraft wings and other objects in air flows.

After we have measured D on the model airplane, how to use the dimensional analysis above to extrapolate it to the drag on the real airplane? If we ensure the same Re in the model experiment as in the flight of the real aircraft, then the pi theorem guarantees that C_d also be the same between the two. Thus, we have achieved similarity, and the drag force D_m measured on the model in the wind-tunnel experiment can be translated to the force D_p on the real airplane according to

$$\frac{D_m}{\rho_m U_m^2 d_m^2} = \frac{D_p}{\rho_p U_p^2 d_p^2},$$

where the subscript m refers to quantities in the model experiment, and p to those for the prototype. The beauty of similarity is that it works without our having to know the relationship between the “output”, i.e., the drag force D in this case, and the input variables and parameters. In reality, such a dependence is usually complex and not known. In chemical and process engineering, this approach forms the foundation for scale-up of bench-top experiments to plant-scale reactors [2, 3]. It has also seen limited applications to bioreactors and living systems [1, 4].

To summarize the above procedure, we go through the following steps:

- (a) Identify the key output function
- (b) Identify the input variables and parameters
- (c) Construct the dimensionless Π groups using dimensional analysis
- (d) Establish similarity-scaling relations.

The same procedure readily applies to the scaling of an organ-on-a-chip (OoC), as an OoC is also a system with one or multiple outputs that depend on input variables and parameters. However, an OoC typically involves both mechanical and biochemical mechanisms, variables and parameters. Thus, it is likely more complex than the typical mechanical system, with a larger number of inputs and outputs. Moreover, greater complexities arise when multiple OoCs (MOoCs) are integrated into a body-on-a-chip system that models the crosstalk between multiple organs. However, this increase in complexity is incremental—a greater number of variables and parameters result in a greater number of Π groups, and greater practical challenges to ensure equality of all these Π groups between the model and the prototype. There is no qualitative difference in applying similarity scaling to MOoCs. In practice, complete similarity becomes rare for such

complex systems, and one may have to rely on partial similarity. The three case studies detailed below consist of two single OoCs and one MOoC.

Data for case study 1: lung-on-a-chip

Huh et al. [5] developed the lung-on-a-chip (LOAC) as a model for an alveolus. It consists of an air chamber and a microvascular chamber separated by a membrane-supported air-liquid interface (ALI). On the air side of the membrane, an epithelium is cultured with airway epithelial cells with proper mucus production. The vascular side of the membrane features an endothelial monolayer. A distinct feature of the device is that the membrane can be cyclically stretched at prescribed amplitude and frequency, thus replicating the alveolar stretching during breathing. Huh et al. [6] explored the use of LOAC as a disease model for pulmonary edema that arises during cancer treatment by interleukin-2 (IL-2). They observed that the concurrence of IL-2 at clinical dosage and stretching at proper frequency, amplitude and duration leads to gradual loss of the barrier function and increased permeability across the ALI (their Fig. 2B). The permeability is quantified by measuring the amount of fluorescein-conjugated inulin that crosses the ALI in time. The increased permeability is a hallmark of acute respiratory distress syndrome [7].

For dimensional analysis of the LOAC, we list the output and input variables:

- Membrane permeability k
- IL-2 volume fraction c
- Membrane stretching strain amplitude ε
- Stretching frequency f
- Duration of IL-2 application T
- Medium perfusion velocity V
- Total thickness of the ALI δ
- Chamber width D

The 8 quantities have 2 fundamental dimensions (length L and time T ; note that permeability has dimension L^2 from Darcy's law), so we expect 6 dimensionless Π groups. They can be constructed methodically using the procedure outline in the above. But we can also take some shortcuts by recognizing that c and ε are dimensionless to begin with, and the other Π groups can be obtained from simple ratios or products:

$$\Pi_1 = k/D^2, \Pi_2 = c, \Pi_3 = \varepsilon, \Pi_4 = Tf, \Pi_5 = fD/V, \Pi_6 = \delta/D.$$

Let us examine the various similarity criteria and determine if they are satisfied in the LOAC. Alveolar diameter ranges from 200 to 500 microns [8], and the LOAC device has a membrane width of $D = 400$ microns. Thus, Huh et al. strove for a 1:1 scale in dimensions. The ALI thickness $\delta \sim 1 \mu\text{m}$ also approximates the in vivo thickness. Thus, all the geometric features are matched to the alveolus, with

identical length ratios: $\Pi_6 = idem$, which is a shorthand for Π_6 being the same between the model and the prototype. The requirement of length ratios to be the same is known as geometric similarity [9]. When applied to cell cultures, the criterion of geometric similarity should be supplemented by morphological similarity, i.e., similar spatial arrangement of the different cell types. In the LOAC, the endothelial-epithelial membrane approximates the air-blood boundary in vivo, with a monolayer of endothelial or epithelial cells in confluence on either side. Therefore, morphological similarity is also satisfied.

Among the operating conditions, Huh et al. [6] have chosen the strain amplitude $\varepsilon = 10\%$ and frequency $f = 0.2$ Hz for the membrane stretching, and the medium perfusion rate V according to in vivo conditions. Thus, $\Pi_3 = idem$ and $\Pi_5 = idem$. These quantities concern the flow and movement, and their similarity is known as kinematic similarity in engineering [9].

The IL-2 dosage c and application time T were also chosen to be the same as in vivo. We can call the similarity among quantities concerning the administration and metabolism of drugs metabolic similarity. Then $\Pi_2 = idem$ and $\Pi_4 = idem$, and metabolic similarity is also observed.

Since all the input Π groups satisfy similarity: $\Pi_i = idem$, $i = 2, \dots, 6$, the membrane permeability must also obey similarity: $\Pi_1 = idem$, or $k = idem$ since $D = idem$. Complete similarity is achieved; in fact, this happens to be a special case with 1:1 scaling. Huh et al. [6] reported good agreement between the in vitro permeability and ex vivo data on whole mouse lung. This serve as a successful example in support of the similarity scaling method.

Data for case study 2: liver-on-a-chip

The Liver-Chip is typical of many liver-on-a-chip devices that have appeared in recent years [10, 11]. As a mimic for a liver sinusoid, the chip's overall design resembles that of the LOAC in having a porous membrane separating two microfluidic chambers. The top (vascular) chamber has liver sinusoidal endothelial cells cultured atop the membrane, and is perfused by liquid medium. The bottom chamber features hepatocytes. In the study to be analyzed here, Ewart et al. [12] injected various drugs into the vascular chamber of the Liver-Chip device to study drug-induced liver injury (DILI). Of several indicators of DILI, the reduction in albumin production is a quantitative marker that can serve as the output in similarity analysis.

As in the above, we first identify the output and input variables:

- The ratio ϕ of albumin production under drug treatment to the baseline of no drugs
- Medium perfusion velocity u
- Initial drug molar concentration c

- Required drug concentration c_{50} to produce a 50% reduction in albumin, as an indication of the drug's potency
- Drug diffusivity in perfusate D
- Drug permeability through membrane P
- Drug clearance rate k
- Chamber dimension L

An obvious choice for the output function is the ratio of albumin production ϕ , which has no dimension to begin with: $\Pi_1 = \phi$. The 7 input quantities contain 3 fundamental dimensions: length L , time T and amount of substance N (the molar concentration has dimension $\{c\} = \{c_{50}\} = NL^{-3}$). Thus we expect 4 Π groups which can be constructed following the standard procedure [1]. But shortcuts are available given the special features of the problem. An obvious Π group is the ratio of concentrations: $\Pi_2 = c/c_{50}$. To construct the remaining 3 Π groups, an intuitive way is to recognize the various time scales in the system:

$T_r = L/u$, residence time;

$T_c = cL^3/(ck) = L^3/k$, clearance time;

$T_d = L^2/D$, diffusion time;

$T_p = L/P$, permeation time.

Now we can obtain the 3 Π groups from the ratios of these time scales: $\Pi_3 = T_d/T_r = uL^2/k$, $\Pi_4 = T_d/T_r = uL/D$, $\Pi_5 = T_p/T_r = u/P$, where Π_3 and Π_4 can be identified respectively with the Damkhöler number and the Péclet number commonly used in chemical engineering processes [13]. In the following, we estimate the parameter values in vitro and in vivo to assess if similarity is achieved.

Geometry and morphology. The Liver-Chip has larger dimensions than the liver sinusoid in vivo, but this need not impair similarity scaling as long as the differing length scale is compensated for by the other parameters such that Π_3 and Π_4 are equal to those in vivo. On the chip, the functional surfaces are essentially planar 2D monolayers, whereas the liver sinusoid has a tubular structure. The difference in shape does not matter as long as the monolayer surface area and the total number of hepatocytes are properly scaled. From the dimension of the Liver-Chip, we have taken the length scale $L = 200 \mu\text{m}$ in vitro [10, 12], compared with the in vivo dimension of $5 \mu\text{m}$ [14]. In terms of cell morphology, the Liver-Chip mimics the heterotypic cellular arrangement, using the proper ratio among the different cell types (e.g., hepatocytes, liver sinusoidal endothelial cells, stellate cells and Kupffer cells), and arranging them in a layered structure that functionally mimics the sinusoid [10, 12, 15]. Based on this, we can argue that morphological similarity is maintained.

Perfusion rate. To ascertain kinematic similarity, we evaluate the in vitro perfusion velocity u from the volume flow rate $Q = 30 \mu\text{L/hr}$ [12] and the cross-sectional area A of the endothelial chamber of the Liver-Chip [10, 12]. This gives us the in

vitro velocity of 2500 $\mu\text{m}/\text{min}$. The in vivo velocity is inferred from the in vitro perfusion velocity of Prodanov et al. [11] and their statement that this velocity “is 2–3 orders of magnitude lower than in vivo values”. We will take an intermediate ratio of 500. Their in vitro velocity is calculated from the perfusion rate $Q = 1 \mu\text{L}/\text{hr}$ and the endothelial cross-sectional area $A = 0.125 \text{ mm}^2$. Thus, the in vivo velocity $u = 66.7 \text{ (mm/min)}$.

Drug clearance rate. The liver clearance rate can differ by up to 2 orders of magnitude among different drugs [16]. For our purpose, we have chosen diclofenac as a representative because its clearance data are available [16, 17] and it is among the drugs tested by Ewart et al. [12]. The in vitro clearance rate for diclofenac is about 17 $\mu\text{L}/\text{min}$ per 10^6 hepatocytes [17]. Then we ask how many hepatocytes are in the Liver-Chip of [12]. The endothelial chamber is 1 mm wide, 0.2 mm deep and 18 mm long [10]. The area of the hepatocyte-covered membrane is $A = 18 \text{ mm}^2$. Given the cell diameter of 13.52 μm [18], the total number of hepatocytes in vitro is $N = 9.85 \times 10^4$. Now the in vitro clearance rate for the Liver-Chip is $k = 1.67 \mu\text{L}/\text{min}$. The in vivo k value for diclofenac is 418 mL/min per kg of human body weight [16]. Taking a 70-kg person with a total number of 1 billion sinusoids [14], we can estimate the in vivo clearance rate for a single sinusoid: $k = 2.93 \times 10^7 \mu\text{m}^3/\text{min}$.

Transport coefficients. For the diffusivity in medium, a representative value for small-molecule drugs is $D = 4.5 \times 10^4 \mu\text{m}^2/\text{min}$ [19]. For the permeability P , Leedale et al. have given a formula for calculating the “passive diffusion uptake” from the lipophilicity of the drug, in unit of $\mu\text{L}/\text{min}$ per 10^6 hepatocytes. For a medium lipophilic drug, we can calculate the permeability through each hepatocyte of diameter of $d = 13.52 \mu\text{m}$ [18], and then through the Liver-Chip with $N = 9.85 \times 10^4$ hepatocytes: $P = 6.53 \times 10^6 \mu\text{m}/\text{min}$. For D and P , we find no in vivo values, and thus have assumed the same values as in vitro.

Dosage. Ewart et al. [12] have tabulated the in vitro and in vivo doses in their Table S2. The c_{50} values for declofenac are taken from Chan et al. [20], which listed $c_{50} = 0.05 \mu\text{M}$ or $0.15 \mu\text{M}$ in two different human whole blood assays. We have taken an intermediate value $c_{50} = 1 \mu\text{M}$.

These parameters are compiled in Table 1 of the main paper. The dimensionless groups show that similarity is achieved between the Liver-Chip and the liver sinusoid. This provides an explanation for the success of the chip in detecting DILI, as well as support to the similarity scaling approach.

Data for case study 3: gut-liver multi-organ-on-chip system

Cirit et al. [16, 17, 21] presented detailed pharmacokinetic data for a number of drugs in a gut-liver MOoC system, which captured the key functions of both organs and their crosstalk. We follow the same procedure as above, first identifying the output and input variables, then constructing the Π groups, and finally determining if the similarity criteria are satisfied.

This MOoC has multiple output variables, alongside a host of input variables:

- The output variables are the time-concentration profiles for drugs in different compartments of the system: $c_{ga}(t)$ in the apical chamber of the gut, $c_{gb}(t)$ in the basolateral chamber of the gut, $c_l(t)$ in the liver, and $c_m(t)$ in the mixing chamber
- Intrinsic drug clearance rates C_g for gut and C_l for liver
- Drug permeability through membrane P
- Fraction of unbound drug in circulating medium f_u
- Total perfusion rate Q , and its partition between the gut and liver
- Initial drug molar concentration c_0 in dosed chamber
- Geometric parameters: volumes V_{ga} (gut apical chamber), V_{gb} (gut basolateral chamber), V_l (liver chamber), V_m (mixing chamber); surface area of the gut membrane S

There are a total of 15 quantities in the list above, with 3 fundamental dimensions (length, time and amount of substance). Thus, we expect 12 dimensionless Π groups [1]. For the output variables, the 4 molar concentrations can be easily scaled to yield 4 Π groups by using the initial drug molar concentration:

$$\Pi_1 = c_{ga}/c_0, \Pi_2 = c_{gb}/c_0, \Pi_3 = c_l/c_0, \Pi_4 = c_m/c_0.$$

For the remaining 10 variables and constants, there are only two fundamental dimensions, length and time. Thus, we can define a characteristic length $L_0 = V_m^{1/3}$ and a characteristic time (the circulation time) $T = V_m/Q$, and readily obtain the remaining 8 dimensionless Π groups:

$$\Pi_5 = f_u, \Pi_6 = C_g/Q, \Pi_7 = C_l/Q, \Pi_8 = PS/Q,$$

$$\Pi_9 = V_{ga}/V_m, \Pi_{10} = V_{gb}/V_m, \Pi_{11} = V_l/V_m, \Pi_{12} = S/V_m^{2/3}.$$

The last one Π_{12} can be dropped since S only appears together with P in the drug mass transport, and thus PS can be viewed as a single parameter in the scaling exercise. In the following we estimate the parameter values in vitro and in vivo to assess if similarity is achieved.

Geometry and morphology. The in vitro geometric parameters are: $V_{ga} = 0.5$ mL, $V_{gb} = 1.5$ mL, $V_l = 1.4$ mL, $V_m = 1$ mL, and $S = 1.12$ cm².

For the liver volume in vivo, we take $V_l = 1500$ mL [22]. There is some uncertainty as to how to interpret the other volumes in vivo. If we equate the gut with the small intestines, with an average length of 5 m [23] and diameter of 2.5 cm [24], we get a gut volume of $V_{ga} = 2454$ mL. Its surface area is $S = 30$ m² because of the surface ruffles due to the villi and microvilli [25]. The “basolateral chamber” of the gut in the OoC corresponds to the intestinal blood vessels, for which we did not find a volume. Thus, we will take V_{gb} to be the same as V_{ga} in vivo. Finally,

the “mixing chamber” should correspond to the systemic circulation for these 2 organs. The total amount of blood in the human body is roughly 5000 mL [26]. Since the liver and the gut account for, respectively, about 25% and 10% of the total cardiac output [27], we can take 35% of the total blood volume to be the in vivo counterpart of the mixing chamber volume: $V_m = 1750$ mL. Based on these values, we can compare the Π groups Π_9, \dots, Π_{12} (in vitro values followed by in vivo values in parentheses):

$$\Pi_9 = 0.5 (1.4), \Pi_{10} = 1.5 (1.4), \Pi_{11} = 1.4 (0.857), \Pi_{12} = 1.12 (2066).$$

The volume ratios $\Pi_9, \Pi_{10}, \Pi_{11}$ are reasonably close between in vitro and in vivo, but the surface area discrepancy (Π_{12}) is large. Since Π_{12} is unimportant to the scaling, as noted in the above, we can claim that the MOoC device has satisfied geometric similarity approximately.

In terms of cell composition and configuration, the MOoC strives to mimic the gut and liver in vivo. For example, the liver OoC used the in vivo ratio between the number of hepatocytes and Kupffer cells. Similarly, the gut OoC used realistic ratios among the epithelial, goblet and dendritic cells. The configuration of the liver OoC reflects the liver sinusoids in vivo, while the gut OoC mimics the epithelium in vivo. Thus, based on the available information, we can assume that morphological similarity is attained.

Drug clearance, transport and liquid perfusion rates. The key quantities are C_g, C_l, P and Q , and these are tabulated for the drug diclofenac in Table 2 of the main paper. The in vitro values are taken from [17]. Maas et al. [16] have cited in vivo values for C_l , but did not report any C_g value. In view of the much lower gut clearance in vitro, the in vivo value is expected to be low, and we have put it to zero. For the permeability P , Maas et al. reported an in vitro value but not an in vivo one. We have taken their in vitro value, which differs somewhat from that of [17], as in vivo. The in vivo perfusion rate is based on the hepatic blood flow [27] coming from both the artery and the portal vein. This is the proper counterpart of the in vitro flow rate in view of the flow rate partition scheme in the MOoC [16, 17].

Drug dosage. The last input Π group to be examined is $\Pi_5 = f_u$, the fraction of unbound drug in the circulating medium. Tsamandouras et al. [17, 21] cited $f_u = 0.13$ in both the gut and the liver in the MOoC device. We have not found in vivo values. If one uses the proper medium in vitro, f_u should be the same as in vivo. Thus, we assume that $\Pi_5 = idem$ is satisfied.

Diclofenac time-concentration profiles. Of the 4 output Π groups, we have in vivo data only for the drug concentration in the plasma [16], which corresponds to the in vitro concentration in the mixing chamber [21]. Both correspond to $\Pi_4 = c_m/c_0$, which is compared in Figure 1 in the main text. To evaluate Π_4 , we need the c_0 values in vitro and in vivo. In vitro, $c_0 = 40$ μ M [21]. In vivo, Maas et al. [16] estimated $c_0 = FD_o/V_{ga}$, F being the drug’s bioavailability, D_o the dose

administered, and V_{ga} the volume of the dosing chamber (apical gut chamber). With $F = 0.54$, $D_o = 50$ mg [28], and $V_{ga} = 2454$ mL, we get the in vivo characteristic concentration in the gut: $c_0 = 11$ $\mu\text{g/mL}$.

In comparing the partial list of Π groups in Table 2, we have come to the conclusion that kinematic similarity is violated. This explains the failure of the liver-gut MOoC to recapitulate the in vivo drug concentration profile of Figure 1. Thus, this case study provides an example of how failing the kinematic similarity leads to failing the metabolic similarity. It illustrates the importance of similarity scaling from a negative result.

Note, however, that the failure being in a multi-organ system is a coincidence; the similarity scaling approach is not intrinsically limited to single-organ OoCs. In practical terms, MOoCs have a greater number of parameters and hence more Π groups. This does make complete similarity harder to achieve and increase the chance of a certain criterion being violated. Partial similarity may become a necessity for MOoCs.

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